

5           **HIGH PERFORMANCE ION MOBILITY SPECTROMETRY USING**  
             **HOURLASS ELECTRODYNAMIC FUNNEL AND INTERNAL ION FUNNEL**

Statement Regarding Federally Sponsored Research Or Development

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Background Of The Invention

The hope of achieving high performance identification of ionic species using ion  
mobility drift tubes coupled with time of flight mass spectrometers has long been held by  
15 those skilled in the art. The general concept has been known since at least the publication  
of the paper entitled "Ion Mobility / Mass Spectrometric Investigation of Electrospray  
Ions" by R. Guevremont, K.W.M. Siu, and L. Ding in the Proceedings of the 44th ASMS  
Conference, p. 1090 (1996). This paper, and all other papers and patents identified herein  
are hereby explicitly incorporated into this disclosure by this reference. The concept was  
20 again published in the paper "Combined ion mobility/time-of-flight mass spectrometry  
study of electrospray-generated ions. Anal. Chem. 69, 3959 (1997). The concept was  
again described in the patent literature in May of 1999, when US Patent 5,905,258 titled  
"Hybrid ion mobility and mass spectrometer" issued to David E. Clemmer, et al.

While the general concept of such systems has thus long been recognized, those  
25 having skill in the art have also recognized limitations associated with the technique  
when put into practice. One approach towards achieving the objective of increased  
sensitivity in ion mobility spectrometry/mass spectrometry (IMS/MS) instruments is  
described in US Patent Application Pub No. 2001/0032929A1 by Fuhrer et al. wherein  
improvements in sensitivity are claimed as a result of preserving a narrow spatial

distribution of migrating ions through the use of periodic/hyperbolic field focusing.

Variations on the general IMS/MS concept are shown in US pat. # 6,323,482 filed 05/17/1999, granted 11/27/2001, "Ion mobility and mass spectrometer" which shows the use of collision cell in an IMS/time of flight MS hybrid system and various means to

5 incorporate the collision cell into such instrumentation. Further variations are also shown in US pat. # 6,498,342 filed 07/13/2000, granted 12/24/2002 "Ion separation instrument" which introduces the liquid-phase separation (such as liquid chromatography) prior to IMS/time of flight MS or a tandem IMS/time of flight MS system. Finally, US pat. # 6,559,441 filed 02/12/2002, granted 05/06/2003 "Ion separation instrument" details  
10 various conceivable versions of tandem IMS, e.g. use of different buffer gases and/or different temperatures.

Despite these and other improvements, problems associated with loss of ions in ion mobility spectrometer (IMS) drift tubes have continued to prevent IMS/MS systems from reaching their full potential as analytical instruments. Rather, other systems with  
15 much slower separations times, but lower ion losses, such as liquid chromatography mass spectrometry (LC/MS), have prevailed despite the sample analysis "throughput" reductions associated with such systems. The problem of excessive ion losses in IMS/MS systems is well known by those having skill in the art, and has repeatedly been identified in the literature by numerous researchers active in the field. For example, in  
20 the paper titled "Gas-phase separations of complex tryptic peptide mixtures" published in Fresenius J. Anal. Chem. 369, 234 (2001), by J.A. Taraszka, A.E. Counterman and D.E. Clemmer, in the sentence bridging pages 242 and 243, the authors described one aspect of the problem thusly: "Currently one stumbling block associated with high-resolution instruments is that most signal (~99-99.9%) is discarded when the short pulse of ions is  
25 introduced into the drift tube." In the paper titled "Multidimensional separations of complex peptide mixtures: a combined high performance liquid chromatography/ion mobility/time-of-flight mass spectrometry approach" published in Intern. J. Mass Spectrom. 212, 97 (2001), by S. J. Valentine, M. Kulchania, C. A. Srebalus Barnes, and D. E. Clemmer, at the final paragraph on page 108, the authors again recognize  
30 difficulties with the technique stating: "It is typical to discard 99-99.9% of the ion signal during the mobility experiment [34]; thus, these experiments are inherently less sensitive

than conventional LC-ESI-MS methods.” Yet another paper in the literature identifying the problem is entitled “Coupling ion mobility separations, collisional activation techniques, and multiple stages of MS for analysis of complex peptide mixtures”, Anal. Chem. 74, 992 (2002), by C. S. Hoaglund-Hyzer, Y. J. Lee, A. E. Counterman, and D. E. Clemmer. At page 1005, the authors state: “We also note that although improvements in sensitivity have been demonstrated, the current technologies are still not as sensitive as the well-developed MS/MS strategies; however we believe that much of this difference will be diminished as additional improvements in the instruments are made. Finally, other authors, including Russell and coworkers active in the field at Texas A&M University, have repeatedly pointed out the need for much better IMS/MS sensitivity.

Thus, there remains a need for methods and apparatus that enable increased sensitivity in ion mobility spectrometry/mass spectrometry (IMS/MS) instruments and which substantially reduces the loss of ions in ion mobility spectrometer (IMS) drift tubes.

#### Brief Summary Of The Invention

Accordingly, it is an object of the present invention to provide methods and apparatus that enable increased sensitivity in ion mobility spectrometry/mass spectrometry instruments and substantially reduce the loss of ions in ion mobility spectrometer drift tubes. These and other objects of the present invention are accomplished by providing a method and apparatus for analyzing ions utilizing an hourglass electrodynamic ion funnel at the entrance to the drift tube and/or an ion funnel at the exit of the drift tube, as shown in the cutaway schematic drawing of Fig. 1. Briefly, the present invention comprises an hourglass electrodynamic funnel 1 formed of at least an entry element 2, a center element 3, and an exit element 4, each of said elements having an aperture. The entry element 2 is aligned such that a passageway for charged particles is formed through the aperture within the entry element 2, through an aperture in the center element 3, and then through the aperture in the exit element 4. It is important that the aperture in the center element 3 is smaller than the aperture of the entry element 2 and the aperture of the exit element 4. Typically, the hourglass electrodynamic funnel 1 will consist of more than three elements, perhaps as many as several hundred elements. It is not necessary that the

center element 3 be at the exact middle of all elements. In an embodiment, for example, with 100 elements, the center element 3 could be the 80<sup>th</sup> element, rendering the electrodynamic funnel asymmetric. All that is required of the center element 3 is that it be the smallest of the elements, and that the center element 3 have at least one element (the entry 2 and exit element 4) to each of both sides. Conceptually, therefore, three elements are the minimum necessary to describe and operate the invention.

The hourglass electrodynamic funnel 1 forms the entrance to a drift tube 5. Ions generated in a relatively high pressure region by an ion source 6 at the exterior of the hourglass electrodynamic funnel 1 are transmitted to a relatively low pressure region at the entrance of the hourglass funnel 1 through a conductance limiting orifice 7, which may be fashioned from, by way of example, a heated capillary. Typically, a differential pump 8 evacuates the hourglass electrodynamic funnel chamber. Alternating and direct electrical potentials are applied to the elements of the hourglass electrodynamic funnel 1 as with a standard ion funnel as described in US Patent 6,107,628, issued August 22, 2000, and entitled "Method and apparatus for directing ions and other charged particles generated at near atmospheric pressures into a region under vacuum" the entire contents of which are hereby incorporated herein by this reference, thereby drawing ions into and through the hourglass electrodynamic funnel 1. In this manner, the hourglass electrodynamic funnel 1 captures an expanding flow of ions generated in a relatively high pressure region and directs them through the small aperture of the center element 3, into the drift tube 5 which is maintained at a relatively low pressure compared to the ion generation region. The center element 3 thus defines a small aperture for the entry to the drift tube 5, and thus a conductance limit. Combined with the entry element 2, this configuration introduces relatively large quantities of ions into the drift tube 5 while maintaining the gas pressure and composition at the interior of the drift tube 5 as distinct from those at the entrance of the electrodynamic funnel 1 and allowing a positive gas pressure to be maintained within the drift tube, if desired.

The electrodynamic funnel 1 may also utilize a jet disturber 9, such as that described in US Patent 6,583,408, issued June 24, 2003 and entitled "Ionization source utilizing a jet disturber in combination with an ion funnel and method of operation" the entire

contents of which are incorporated herein by this reference. The jet disturber **9** can be operated to prevent undesired species from entering the drift tube **5**, to modulate the signal intensity, and to improve the signal to noise ratio. Additionally, the hourglass electrodynamic **1** funnel can include a further means **10** for temporarily containing the flow of ions out of the aperture of the exit element. These means could be a plurality of wires, a mesh, or a microchannel plate. Ions can be accumulated in the region between the center element **3** and the exit element **4**, and by varying the potential applied to these means, pulsed through the exit element **4** at a known time, thereby allowing precise analysis of the time necessary for differing ions to pass through the flow tube. The hourglass shape of the electrodynamic funnel **1** thus allows the accumulation of much larger numbers of ions than is enabled by the conventional geometry of prior art ion funnels.

Alternatively, ions passing through electrodynamic funnel **1** may be pulsed by intermittent deflection by an electric field orthogonal to the ion path, generated by any of several means **10** known in the art, including, but not limited to, a Bradbury-Nielsen gate, two or more deflection plates, or a split lens.

While the apertures are typically circular, they may be any shape. For specific applications, for example to form ion packets having an elongated profile, and particularly a highly elongated “razor” profile, as is useful for field asymmetric waveform ion mobility spectrometry, photodissociation, and laser spectroscopy, ellipsoidal and rectangular apertures are preferred.

The exit of the drift tube **5**, located at the opposite end of the drift tube from the hourglass electrodynamic funnel **1**, is typically in communication with an ion analysis means **11**, such as a mass spectrometer. While not meant to be limiting, the method and apparatus of the present invention can be in communication with a quadrupole mass spectrometer, a time of flight mass spectrometer, a Fourier-transform ion cyclotron resonance mass spectrometer, a photoelectron spectrometer, or a photodissociation spectrometer. The drift tube **5** can be an ion mobility spectrometer, a field asymmetric waveform ion mobility spectrometer, a selected ion flow tube, or a proton-transfer reaction mass spectrometer.

The present invention is capable of being interfaced with any conventional ion source 6, including but not limited to electrospray ionization, coldspray ionization, thermospray ionization, matrix-assisted laser desorption ionization, surface-enhanced laser desorption ionization, laser vaporization, and arc discharge.

5 The present invention may also be configured as having two or more hourglass electrodynamic funnels 1 each forming a separate entrance to the drift tube 5 thereby providing two or more passageways for ions generated in a relatively high pressure region at the exterior of the drift tube 5 to a relatively low pressure region at the interior of the drift tube 5. In this manner, the ease of calibration of the present invention is  
10 enhanced.

The present invention may also be configured as a dual entry hourglass electrodynamic funnel as described in US Patent Application Serial No. 10/400,356, filed March 25, 2003, and entitled "Multi-Source Ion Funnel," now US Patent \_\_\_\_\_, the entire contents of which are incorporated herein by this reference. As shown in the  
15 Multi-Source Ion Funnel patent application, the dual source ion funnel is formed of at least two entry elements, one center element, and one exit element, each of the elements having an aperture, and wherein each of the two or more entry elements are aligned such that a passageway for charged particles is formed through apertures within the entry elements, through an aperture in said center element, and through the aperture in the exit  
20 element, thereby providing two separate but merging passageways for ions generated in a relatively high pressure region to a relatively low pressure region. As adapted for the present invention, as with the more general case, the aperture of the exit element 5 of the dual source configuration is again larger than each of the apertures of each of the center elements 3, and the two separate but merging passageways are for ions generated in a  
25 relatively high pressure region at the exterior of a drift tube 5 to the relatively low pressure region at the interior of the drift tube 5.

In another aspect of the present invention, an internal ion funnel 12 is provided within the drift tube 5. The internal ion funnel 12 is configured as a standard ion funnel; it has at least one element 13 having a relatively small aperture and at least one element having a  
30 relatively large aperture 14. Alternating and direct electrical potentials are applied to the

elements of the internal ion funnel 12 as with a standard ion funnel as described in  
“Method and apparatus for directing ions and other charged particles generated at near  
atmospheric pressures into a region under vacuum,” US Patent 6,107,628, issued August  
22, 2000. As with the hourglass electrodynamic funnel 1, the internal ion funnel 12 will  
5 typically consist of more than two elements, perhaps as many as 100 elements.

Conceptually, however, as is the case with the standard ion funnel, two elements are the  
minimum necessary to operate internal ion funnel 12. The internal ion funnel 12 is  
positioned at the exit of said drift tube 5 wherein the element having the small aperture 13  
is positioned adjacent to the exit of drift tube 5. The internal ion funnel 12 may be used  
10 alone or in combination with any of the aforementioned variations of the hourglass  
electrodynamic funnel 1. The advantage of the internal ion funnel 12 is that ions that are  
usually dispersed away from the exit aperture within the drift tube 5, such as those that  
are typically lost in conventional drift tubes to any subsequent analysis or measurement,  
are instead focused through the exit of the drift tube 5, vastly increasing the amount of  
15 ions exiting the drift tube 5.

While the general characteristics of the present invention have been shown and  
described, the operation and advantages of the present invention are best illustrated by an  
example. Accordingly, experiments in which the present invention was reduced to  
practice and then operated to demonstrate the superior performance enabled by the  
20 present invention when compared to prior art methods were conducted and are described  
below. However, the present invention should in no way be viewed as limited to either  
the specific device, or the operation of that device, as described below. Rather, these  
experiments are provided merely to illustrate the advantages of the present invention, and  
to illustrate an example of how the present may be reduced to practice and operated.  
25 Those having skill in the art will readily recognize that numerous departures from the  
specific details of the device and its operation shown below are possible, yet would still  
fall well within the more general description provided above, and set forth in the  
appended claims.

30 Brief Description Of The Several Views Of The Drawing

FIG. 1 is a schematic cut away drawing of the present invention.

FIG. 2 shows an hourglass electrodynamic funnel and an internal ion funnel built to demonstrate a preferred embodiment of the present invention.

FIG. 3 is a drift tube built to demonstrate a preferred embodiment of the present invention.

FIG. 4 is a mass-spectrum of Glu-Fibrinopeptide (1572 amu) from a commercial (prior art) Micromass system.

FIG. 5 is a mass-spectrum of Glu-Fibrinopeptide (1572 amu) from a commercial (prior art) Micromass system fitted with a standard ion funnel at the ESI/MS interface.

FIG. 6 is a mass-spectrum of Glu-Fibrinopeptide (1572 amu) passed through the hourglass electrodynamic funnel, the IMS drift tube, and the internal ion funnel described in the preferred embodiment of the present invention.

FIG. 7 is a mass-spectrum of Insulin (5734 amu) from a commercial (prior art) Micromass system

FIG. 8 is a mass-spectrum of Insulin (5734 amu) from a commercial (prior art) Micromass system fitted with a standard ion funnel at the ESI/MS interface.

FIG. 9 is a mass-spectrum of Insulin (5734 amu) passed through the hourglass electrodynamic ion funnel, the IMS drift tube, and the internal ion funnel described in the preferred embodiment of the present invention.

## Detailed Description Of The Invention

A device was constructed to demonstrate the advantages and application of the present invention consisting of three sections: an ion source, and ion mobility spectrometer (IMS) drift tube for spatial ion separation, and a mass spectrometer for mass analysis of separated ion packets. Except as noted below, the device utilized the general



arrangement of each of these components as shown in the conceptual drawing shown in Figure 1. While all voltages listed below are for positively charged ions (cations), those having skill in the art will readily recognize that the polarities can readily be inverted to analyze negatively charged ions (anions).

5        This ion source section comprises an electrospray ionization (ESI) source that generates solvated ions, a heated capillary that desolvates them, and an hourglass electrodynamic (ED) ion funnel that further desolvates and focuses them into IMS. The ESI and the heated capillary were standard instruments available commercially from Waters/Micromass, Finnegan, and other mass spectrometer (MS) equipment  
10       manufacturers.

      In the operation of the device, an ESI needle delivered the analyte solution pumped by a syringe pump through a capillary. Ions generated in ESI were sampled into a heated capillary with the internal diameter of  $\sim 0.5$  mm and length of  $\sim 10$  cm. To desolvate ions by thermal heating, this capillary was kept at  $\sim 120^{\circ}\text{C}$  by resistive heaters  
15       under a closed-loop control using a thermocouple.

      Ions exiting the capillary were sampled into an hourglass ED funnel. Like a regular ion funnel in the prior art, the hourglass ED funnel consists of a stack of  $\sim 100$  metal plates alternating with plastic plates for insulation and precise spacing, both plates  $\sim 0.5$  mm. thick for the total funnel length of  $\sim 10$  cm. Each plate has a round hole in the  
20       center, with the i.d. varying between 25 mm and 2 mm.

      Each metal plate features two pins on opposite sides, supplying the RF and DC potentials from the adjoining electrical connectors. The stack is held together and aligned by four parallel ceramic tubes with bolts inside, and is shown in Fig. 2. The bolts secure the funnel to a plastic (herein peek) disk of the first IMS unit, as described below.

25       In a regular funnel of prior art, the i.d. of plate holes decreases (or, for certain plates, remains constant) as the ions travel through. In the hourglass funnel disclosed herein, the i.d. decreases over a number of plates (here from 25 mm to 2 mm over 80 plates), then increases (here to  $\sim 12$  mm over the next 20 plates). The last funnel plate carries only a DC potential (no RF). This plate may be covered with a mesh (here 1 mm.  
30       square mesh) to trap ions. In another embodiment, two last plates carry a DC voltage

only. As with a regular funnel, an hourglass funnel may feature (in the 1<sup>st</sup> section of decreasing plate holes) a DC-only plate with a jet disruptor for ion intensity control.

Typical DC voltages on the ion source elements for the experiments described herein were (with respect to the IMS entrance potential): ESI needle (~ 1.3 kV), heated capillary (220 V), first funnel plate (200 V), jet disruptor (175 V), last funnel plate carrying an RF potential (40 V). The potential of last (DC-only) plate is periodically switched between the “closed” state (ions are trapped in the funnel) and “open” state (a packet of ions released into IMS) by a rectangular DC pulse of desired length. Here, the voltages were 30 V and 100 V for open and closed states, respectively.

As shown in Fig. 3, the drift tube built for these experiments has a modular design, comprising an arbitrary number of nearly-identical units (in this instrument, up to seven). Each unit is housed within a chamber, here a cylindrical steel tube ~ 20 cm. in diameter and 20 cm. long with wall thickness of ~ 2 mm. To join the units, each chamber features welded flanges on both ends, here standard 11-inch 8-bolt flanges with O-ring grooves. Some chambers are fit with insulated high-voltage feedthroughs and/or gas lines. Chambers are insulated and spaced apart by plastic (here ultra high molecular weight polyethylene or peek) disks ~ 1 cm. thick and ~ 30 cm. in diameter, and fastened by insulating bolts and nuts (here fiberglass-reinforced plastic). These disks have central holes to pass ions between units, and other holes and grooves for electrical connections, alignment, and securing the rods described below.

Each unit includes a stack of thin metal rings (here 21 pieces) positioned and aligned on four parallel ceramic rods (here ~ 3 mm. in diameter), and insulated and spaced by plastic spacers. Here, rings with the i.d. of ~ 55 mm and o.d. of ~ 80 mm are spaced ~ 10 mm apart. In one embodiment, one or more rings immediately adjacent to the front ED funnel have a smaller i.d. close to the exit funnel diameter (here ~12 mm), which may improve the ion transmission into the IMS. The assembly is held between two plastic disks by insertion of rods into blind holes in the disks. Rings of any unit are consecutively connected by high-resistance resistors (here 1 MOhm), with same resistances between the units. The median (here 11<sup>th</sup>) ring of each unit is electrically shorted to the chamber wall. The first and last rings of the whole tube are connected to outside voltages through feedthroughs.

At the entrance to the drift tube, the ED funnel is mounted on the plastic disk of first unit as described above, so the last funnel plate is ~ 1 cm. away from the first IMS ring. At the exit to the drift tube, an internal ion funnel is affixed to the plastic disk of last unit. The internal ion funnel is identical to the ED funnel described above, except that it does not exhibit the hourglass shape, contains no jet disruptor, and its mouth is 50 mm in diameter. Voltages applied to the elements of internal ion funnel also mirror those for the ED funnel.

The drift tube contains buffer gas (here He or N<sub>2</sub>) supplied through lines on the last section. In one embodiment, a cylindrical ring is inserted inside the chamber to let the gas in via a laminar, axially symmetric flow avoiding jet formation and turbulence. The pressure inside is monitored using a capacitance manometer (baratron). In the design built for these experiments, the pressure inside can be varied from 1.5 to 22 Torr using a flow regulator. As will be apparent to those having skill in the art, higher pressures (up to 1 atm) would be attainable with smaller funnel apertures, extra stages of differential pumping, greater pumping capacity in the mass spectrometer (below), or some combination thereof.

The drift voltage was loaded on the first IMS ring by a high-voltage DC power supply with a 50 kV range, monitored by a custom-made HV probe. This supply features a circuit that stabilizes the voltage output, and is current-limited for safety reasons. Other voltages routed to the elements of the ion source are provided by smaller supplies floated on top of the drift voltage. This includes the RF waveform on the ED funnel, supplied by an insulation transformer. The drift voltage is partitioned linearly across the IMS length by the resistor chain described above. The chamber of each unit assumes the voltage of its median ring, thus minimizing the likelihood of electrical breakdown through the gas. To ensure the operator safety, exposed high voltages were contained within a grounded metal cage with controls and interlocks on the access doors.

The MS analysis of ion packets separated in IMS was performed by a commercial time-of-flight mass-spectrometer (Waters/Micromass "Ultima", the original version including the ion tunnel). This was used as supplied by the manufacturer, with certain modifications. The front part containing the heated capillary was removed and replaced by a custom-built steel chamber that contains the ED funnel. Like the block of

Micromass, this chamber is grounded. The OEM time-to-digital converter (TDC) was replaced by an Ortec<sup>TM</sup> TDC with a significantly improved performance. In another embodiment, an analog-to-digital (ADC) averager may be substituted for the TDC. This may be beneficial to extend the dynamic range in some regimes, for example at high signal intensities. The manufacturer's software designed for acquisition and processing of mass spectra has no time resolution, and thus was not used with the IMS separation. To record individual ToFMS spectra along the IMS axis, replacement software was coded, providing the data archival and display in two dimensions.

The preferred embodiment described above was then operated to generate the mass-spectra shown in Figures 4-9. These systematically compare the signal intensity in the commercial Micromass system, the commercial Micromass system fitted with a standard (non-hourglass) ED funnel upfront, and the IMS/MS setup described above. As shown in the spectra, the preferred embodiment achieved exceptional ion transmission efficiency. The comparison is made for two peptide ions - a relatively small (Glu-Fibrinopeptide, 1572 amu) and large (Insulin, 5734 amu) that roughly bracket the range of peptide masses relevant to routine proteomic analyses. The ESI operational conditions (noted on the spectra) are typical for calibration protocols standard in the bioanalytical applications industry. For both peptides, the signal intensity in present IMS/MS arrangement is within a factor of two of that for MS analysis only (without IMS). This is an accepted variance due to day-to-day (random) variations in poorly controlled ESI source conditions on the same instrument. Hence, within the error margin normal for such calibrations, there is essentially no measurable ion loss in the IMS stage.

## CLOSURE

While a preferred embodiment of the present invention has been shown and described, it will be apparent to those skilled in the art that many changes and modifications may be made without departing from the invention in its broader aspects. The appended claims are therefore intended to cover all such changes and modifications as fall within the true spirit and scope of the invention.